

METHOD AND APPARATUS FOR GENERATING RANDOM SIGNALS

5 This invention relates to a method and apparatus for generating random signals, and particularly but not exclusively random binary waveforms.

10 Random binary waveforms with specific correlation properties are required for ranging and other applications, especially in radar systems. It is particularly desirable to provide random binary waveforms with maximum unpredictability, hence with low probability of intercept, and also resistant to intelligent jamming. Furthermore, such random binary waveforms are also useful for applications in multi-user environments where many similar or disparate systems operate in the same geographical region and those systems share, at least partly, the same wide frequency band.

15 The generation of binary waveforms with specified correlation properties is of considerable practical interest in the field of radar and communications. For example, in low probability of intercept (LPI) radar the phase of the coherent carrier is modulated by a pseudo-random binary waveform to spread the spectrum of the transmitted signal. In some applications, such as collision avoidance/obstacle detection, altimetry, autonomous navigation etc., many similar radar systems should be capable of operating in the same region and sharing the same wide frequency band. To avoid mutual interference, each system should use a distinct signal, preferably orthogonal to the signals
20 employed by all other systems. Therefore, the successful use of coded-waveform radar in a multi-user environment depends on the availability of large families of waveforms, each with specified correlation properties and
25 low cross correlation values.

An important class of synchronous binary waveforms can be obtained from suitably constructed binary sequences, such as pseudo-random binary sequences. However, when the number and type of systems (co-operating or unco-operating) sharing the same frequency band is unknown and often cannot even be predicted, it is not possible to assign a distinct binary sequence to each of them. It is also difficult to construct large sets of long pseudo-random sequences that provide a significant improvement over purely random sequences.

The above problems can be avoided, or at least alleviated, when asynchronous random binary waveforms are used. In dense signal environments asynchronous waveforms are known to be superior to synchronous ones as a result of the additional randomisation of the zero crossing time instants. Because purely random binary waveforms exhibit maximum unpredictability, they are less vulnerable to intercept and intelligent jamming.

One convenient and inexpensive method to generate a random binary waveform is based on level crossings of a random signal generated by a physical noise source. Fig. 1 shows an example of a generator of a random binary waveform. The generator comprises a physical noise source (PNS) and a zero-crossing detector (ZCD) which can be a comparator or a hard limiter. Fig. 2 shows a typical realisation of a noise signal $s(t)$ and a random binary waveform $b(t)$ obtained from that noise signal and defined by zero crossings of that signal. Each zero crossing results in an event (an edge) in the binary waveform $b(t)$, the events occurring aperiodically and unpredictably.

In radar and also other applications the shape of the correlation function of a binary waveform is of primary importance. The ideal correlation function would have the form of an impulse (Dirac delta) function. In practice, the correlation function of a 'good' binary waveform should attempt to

approximate in some way this ideal shape. Fig. 3 shows the shape of the correlation function $R_b(\tau)$ of a random binary waveform $b(t)$ ideal for ranging applications.

5 In practice it is relatively easy to generate noise signals with a Gaussian distribution, e.g., by exploiting thermal noise. When an underlying noise signal $s(t)$ has a Gaussian distribution, the correlation function $R_b(\tau)$ of a binary waveform $b(t)$ obtained from zero crossings of the signal $s(t)$ can be determined from Van Vleck's formula

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$$R_b(\tau) = (2/\pi) \arcsin[R_s(\tau)]$$

where $R_s(\tau)$ is the correlation function of the underlying noise signal $s(t)$. Therefore, in order to obtain a narrow correlation function $R_b(\tau)$ of a random
15 binary waveform $b(t)$, the correlation function $R_s(\tau)$ of an underlying noise signal $s(t)$ should also be narrow. Because the correlation function and the power spectral density of a random signal form a Fourier pair, a physical noise source utilised to generate a binary waveform with a narrow correlation function should produce a noise signal with an extremely wide frequency
20 spectrum.

It is known that the correlation function of a random binary waveform, not necessarily obtained from a Gaussian noise signal, has a cusp at the origin and that this cusp is sharper when the average number, N_0 , of zero crossings in
25 unit time is larger. When an underlying noise signal $s(t)$ has a Gaussian distribution, the average number, N_0 , of zero crossings in unit time can be determined from Rice's formula:

$$N_0 = B/\pi$$

where B_s is the angular root-mean-square (rms) bandwidth (measured in radians per second) of signal $s(t)$. Consequently, when a Gaussian noise signal $s(t)$ is employed to generate a random binary waveform $b(t)$, it is not possible to reduce the width of the correlation function $R_b(\tau)$ of the binary waveform
5 by means other than the increase in the rms bandwidth B_s of the underlying noise signal $s(t)$. Unfortunately, the generation of ultra wideband noise signals is very difficult in practice.

It would, accordingly, be desirable to provide an apparatus and method for
10 the generation of a random binary waveform with an extremely narrow correlation function suitable for ranging and other applications.

It would also be desirable to provide an apparatus and method for the generation of a random binary waveform intended for application in multi-
15 user environments.

It would be further desirable to provide an apparatus and method for the generation of a random binary waveform resistant to deliberate intelligent jamming.
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It would additionally be desirable to provide an apparatus and method for the generation of a random binary waveform with low probability of intercept.

According to one aspect of the invention there is provided a method of
25 generating a resultant signal containing time marks, referred to herein as events, which occur at random intervals, the method comprising generating a plurality of preliminary signals each containing events occurring at random intervals and combining the preliminary signals. The combining is performed in such a way as to preserve, at least substantially, the events therein. In the
30 embodiments described below, the combining is performed by multiplying (in

either the analog or digital domain) and results in the interspersing of the events in the resultant signal. At least one of the preliminary signals contains events occurring asynchronously (i.e. without being clocked, and indeed the system of the present invention does not depend on the use of a clock).

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Throughout the present specification, including the claims, except where the context indicates otherwise, the term "random" is intended to cover not only purely random, non-deterministically generated signals, but also pseudo-random, deterministic signals such as the output of a shift register arrangement provided with a feedback circuit as used in the prior art to generate pseudo-random binary signals, and chaotic signals. Preferably, however, at least one of the preliminary signals is purely random (non-deterministic), or possibly chaotic, and contains aperiodic events.

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According to a further aspect of the invention, a method of generating a random signal comprises producing a plurality of preliminary signals of random amplitude which can be level-detected to generate a binary waveform with transitions at random intervals, and combining the signals either before or after level-detection in order to generate a resultant random binary output.

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The combining of the signals is performed in such a manner that the events represented by the transitions are, at least partly, preserved. The preliminary signals are, at least partly, uncorrelated.

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Some of the signals or binary waveforms to be combined can be obtained from a single signal or a single binary waveform by utilising a plurality of suitably time-delayed replicas of this signal or waveform. The time-delayed replicas should be, at least partly, uncorrelated with each other, and to this end the time delay used to form each replica preferably has a value which corresponds to a substantially zero level of the correlation function of the original signal.

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In another embodiment, the plurality of preliminary signals are derived from a common physical noise source which produces an output of random amplitude. Each preliminary signal is derived by level-detection, at a
5 respective, different level, of the output of the physical noise source. The levels are preferably separated sufficiently so as to avoid significant correlation between the preliminary signals.

Arrangements embodying the invention will now be described by way of
10 example with reference to the accompanying drawings, in which like reference symbols represent like integers, and in which:

Figure 1 shows an example of a system for generating a random binary
15 waveform in accordance with the prior art;

Figure 2 shows a typical realisation of a noise signal $s(t)$ and a random binary
20 waveform $b(t)$ obtained from that noise signal and defined by zero-level crossings of that signal;

Figure 3 shows the shape of the correlation function $R_b(\tau)$ of a random binary
25 waveform $b(t)$ ideal for ranging applications;

Figures 4 to 6 are block diagrams of, respectively, first to third embodiments
30 of a system according to the present invention;

Figure 7 is a block diagram of a specific example of the embodiment shown in
Fig. 6;

Figure 8 shows the correlation function of a random binary waveform
35 generated by the embodiment of Figure 7;

Figure 9 is a block diagram of yet another embodiment of a system according to the present invention;

5 Figure 10 is a block diagram of a specific example of the embodiment shown in Fig. 8;

Figure 11 is a block diagram of another embodiment of the present invention;

10 Figure 12 is a block diagram of a further embodiment of the present invention; and

Figure 13 shows the correlation function of a random binary waveform generated by the embodiment of Figure 11.

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Fig. 4 shows a system according to the present invention that comprises a plurality of wideband physical noise sources (PNS) followed by spectrum-shaping filters (SSF), a plurality of analog multipliers (AM) or balanced modulators, and a single zero-crossing detector (ZCD) which can be a
20 comparator or a hard limiter. A random binary waveform (RBM) useful for modulating a carrier prior to transmission in radar and communications applications is obtained at the output of the zero-crossing detector (ZCD).

25 Preferably the physical noise source (PNS) is a Zener diode used as *per se* known in the prior art, which provides an output having a Gaussian voltage distribution.

Preferably the zero-crossing detector (ZCD) is a fast comparator with a zero threshold.

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In operation, each physical noise source (PNS) produces a waveform similar to that shown at $s(t)$ in Figure 2, the waveforms being uncorrelated. Each waveform is filtered by a respective spectrum-shaping filter (SSF) which may have an approximately Gaussian power transfer function $|H(\omega)|^2$ of the form:

$$|H(\omega)|^2 = \text{const} \exp(-\omega^2/2B_s^2)$$

where B_s is the angular rms bandwidth.

The advantage of such a characteristic is that the Fourier transform exhibits a monotonic decline to zero level, and thus exhibits no undershoot or ringing. Other types of transfer functions, preferably exhibiting similar advantages, could alternatively be used. It is possible to use filters with identical characteristics for the respective channels (noise sources), or if desired different characteristics could be selected, or indeed in some circumstances the filters could be omitted.

The outputs of the first two filters are multiplied by the first of the analog multipliers (AM), the output of which is multiplied by the output from the third filter (SSF) in the next analog multiplier (AM), etc. The output from the final analog multiplier (AM) is also a waveform generally similar to $s(t)$ in Figure 2 except that there is a substantially greater number of zero-crossings. In effect, the number of zero-crossings is the sum of the number in each of the respective signals from the noise sources (PNS). This output signal is delivered to the zero-crossing detector (ZCD) to produce the random binary waveform (RBM), similar to that shown at $b(t)$ in Figure 2 but again containing a substantially greater number of transitions.

As a result of this arrangement, assuming that there are n channels, the number of zero-crossings in unit time as compared with a single noise source is increased by a factor of n , thus producing a substantially sharper correlation

function and therefore a signal which is much better suited to ranging applications, for example. The rms bandwidth, however, is increased by only \sqrt{n} .

- 5 Although increasing the number of channels also increases the sharpness of the correlation function, the extent of the improvement reduces with an increase in the number of channels. By way of example, assume that each spectrum-shaping filter has an approximately Gaussian power transfer function $|H(\omega)|^2$ of the form:

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$$|H(\omega)|^2 = \text{const} \exp(-\omega^2/2B_s^2)$$

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where B_s is the angular rms bandwidth of the filter. The table below shows the reduction in the half-height width of the correlation function of a random binary waveform as a function of the number of combined channels.

Number of identical channels combined	Half-height width of the correlation function (normalised units)
1	1.00
2	0.56
3	0.39
4	0.30
5	0.25
6	0.21
7	0.18
8	0.16

- 20 In practical embodiments, it is likely that the optimum number of channels would be three or four, as the cost of increasing the number of channels is unlikely to justify the added improvement in the signal.

In the embodiments to be described below, similar considerations apply to the preferred nature of the physical noise sources (PNS), the spectrum-shaping filters (SSF) and the zero-crossing detector (ZCD), and to the number of channels.

Fig. 5 shows another system according to the present invention that comprises a single wideband physical noise source (PNS) followed by a spectrum-shaping filter (SSF), a plurality of analog delay lines (DL), a plurality of analog multipliers (AM) or balanced modulators, and a single zero-crossing detector (ZCD) which can be a comparator or a hard limiter. A random binary waveform (RMB) is obtained at the output of the zero-crossing detector (ZCD).

Figure 5 differs from the arrangement shown in Figure 4 by virtue of the fact that, instead of using independent noise sources (PNS), a single noise source (PNS) is used, the remainder of the preliminary noise signals being produced by time-delayed replicas of the original noise signal, the delays being produced by the analog delay lines (DL). In order to ensure that the noise signals delivered to the analog multipliers (AM) are substantially uncorrelated, each delay line imparts a sufficiently long delay; the delay is such that the correlation function of the signal produced is substantially zero at that delay point. The delays may be different from each other, and/or may vary with time.

Fig. 6 shows yet another system according to the present invention that comprises a plurality of physical noise sources (PNS), each followed by a spectrum-shaping filter (SSF) and a zero-crossing detector (ZCD). The binary waveforms obtained at the outputs of the zero-crossing detectors (ZCD) are then fed to a suitable multi-input-single-output combiner (MIC) that processes

those waveforms in such a manner that their respective zero crossings are, at least partly, preserved. A random binary waveform (RBM) is obtained at the output of the combiner (MIC).

5 Figure 6 differs from the arrangement shown in Figure 4 in that the noise signals are converted into binary signals, by the zero-crossing detectors (ZCD), before being combined.

10 Fig. 7 shows a specific example of the system of Fig. 6 where the combiner (MIC) is formed by a plurality of suitably connected Exclusive-OR logic gates (XOR). These gates, as is well known, perform a binary multiplying operation.

15 Figure 7 represents a preferred embodiment of the invention, assuming that the number of physical noise sources is equal to four. In one particular example of this embodiment, assume that the rms bandwidth measured in Hertz (i.e., $B/2\pi$) of the output of each noise source (PNS) is equal to 25 MHz. For the purpose of this analysis it is also assumed that zero-crossing detectors and Exclusive-OR gates have infinitely fast responses. The half-
20 height width of the correlation function of a binary waveform obtained at the output of any of the zero-crossing detectors is equal to 10.6 ns. However, the half-height width of the correlation function of the resulting binary waveform obtained at the output of the system is equal to 3.2 ns

25 Fig. 8 shows at A the auto-correlation function of the noise signal produced by a single physical noise source (PNS). B represents the correlation function of the binary waveform at the output of the zero-crossing detector (ZCD). C shows the auto-correlation function of the random binary waveform at the output of the embodiment of Figure 7, obtained by combining four

uncorrelated binary waveforms. It will be seen that the correlation function C is much sharper than either of the functions A and B.

Fig. 9 shows yet another system according to the present invention that comprises a single physical noise source (PNS) followed by a spectrum-shaping filter (SSF) and a zero-crossing detector (ZCD), a plurality of binary delay lines (BDL) and a suitable multi-input-single-output combiner (MIC) that processes the waveforms in such a manner that their respective zero crossings are, at least partly, preserved. A random binary waveform (RBM) is obtained at the output of a combiner (MIC).

This is thus similar to the embodiment of Figure 6, except (analogously to Figure 5) the separate noise sources are replaced by delay lines.

Fig. 10 shows a specific example of the system shown in Fig. 9 where the combiner (MIC) is formed by a plurality of suitably connected Exclusive-OR logic gates (XOR).

Figure 11 shows another embodiment of the present invention, in which the output of a physical noise source (PNS) is applied to three level detectors (LD), each of which is arranged to change the state of its output when the signal from the noise source crosses a respective threshold level T1, T2 or T3. The outputs of the level detectors (LD) are combined by Exclusive-OR (XOR) circuits, as in the embodiment of Figure 10, to produce the resultant random binary waveform (RBM). The threshold levels T1, T2 and T3 are separated sufficiently to avoid significant correlation between the outputs of the level detectors (LD). Of course, instead of having level detectors which operate using different threshold levels, it would be possible to use level detectors with a common threshold level, such as zero-crossing detectors, if varying

amounts of DC shift are applied to the output of the physical noise source before the respective level detection operations.

5 Some of the physical noise sources (PNS) referred to above may be replaced by other physical sources utilised to generate chaotic signals, and some, but not all, by other deterministic pseudo-random sources.

Fig. 12 is a functional block diagram of another random binary waveform generator representing another preferred embodiment of the present invention.
10 The system consists of four channels; each of three identical channels comprises a wideband physical noise source (PNS), a spectrum-shaping filter (SSF) and a zero-crossing detector (ZCD).

The fourth channel comprises a pseudo-random binary sequence generator (PRBS) driven by a clock unit (CLK) whose frequency may be constant or
15 may vary. Preferably the pseudo-random binary sequence generator (PRBS) is a shift register with a feedback circuit constructed in accordance with the prior art. A random binary waveform is obtained at the output of the last gate (XOR) of the cascade. Although the correlation function of a pseudo-random
20 binary sequence is periodic, the correlation function of the resulting random binary waveform is aperiodic.

In one example of the arrangement of Figure 12, assume that the rms bandwidth measured in Hertz (i.e., $B/2\pi$) is equal to 15 MHz. For the purpose
25 of this analysis it is assumed that zero-crossing detectors and Exclusive-OR gates have infinitely fast responses. It is also assumed that the pseudo-random binary sequence generator (PRBS) is driven by a clock with frequency of 66 MHz. The pseudo-random binary sequence generator (PRBS) consists of seven stages with a suitable feedback to obtain a sequence of length 127. The
30 half-height width of the correlation function of a binary waveform obtained at

the output of any of the zero-crossing detectors is equal to 17.6 ns. However, the half-height width of the correlation function of the resulting binary waveform obtained at the output of the system is equal to 5.2 ns.

5 Fig. 13 shows at A the auto-correlation function of the output signal produced by a physical noise source (PNS) of the embodiment of Figure 12. B represents the correlation function for the pseudo-random binary sequence (PRBS). C is the correlation function for the binary waveform obtained by combining the three uncorrelated binary waveforms derived from the physical
10 noise sources (PNS). D is the correlation function for the output of the Figure 12 embodiment, which is produced by combining the three uncorrelated binary waveforms from the physical noise sources with the output of the pseudo-random binary sequence (PRBS).

15 The correlation function for the output of a physical noise source (PNS) exhibits tails which extend to plus and minus infinity. This also applies to the binary waveform derived therefrom, and to the combination of the binary waveforms derived from the physical noise sources (PNS). However, the correlation function for the pseudo-random binary sequence (PRBS) exhibits
20 defined upper and lower temporal limits (within the range shown in Figure 13). This therefore also applies to the correlation function D for the output of the Figure 12 embodiment, because this combines the binary waveforms derived from the physical noise sources (PNS) with the pseudo-random binary sequence (PRBS) by Exclusive-OR'ing. This can have significant benefits, for
25 example when the random binary waveform (RBM) is used for modulating carrier signals in radar or similar applications, because placing limits on the range of the auto-correlation function aids in the design of the system.

The invention thus provides a way of obtaining a random binary waveform
30 with a sharp correlation function. This is achieved in the preferred

embodiments by generating Gaussian signals and combining them in a non-linear manner in order obtain a non-Gaussian signal which is used to produce the random binary waveform. Various modifications are possible. The various features disclosed in respect of specific embodiments, particularly the techniques used for producing the preliminary signals which are then combined, can also be used in the other embodiments.

A random binary waveform generator in accordance with the present invention is particularly suited for use in a time delay determination system according to International Patent Application No. WO 00/39643, filed 24 December 1999, the contents of which are incorporated herein by reference.